- An illumination optical system for guiding light from a light source unit to an image display light valve element, wherein at least one curved mirror is disposed in an optical path of said illumination optical system.
 - An illumination optical system according to claim 1, wherein said 2. curved mirror forms a part of a curved surface having rotational symmetry about a predetermined axis.
 - An illumination optical system according to claim 1, wherein said 3. curved mirror is a parabolic mirror.
 - An illumination optical system agcording to claim 3, wherein said parabolic mirror has a form, in a cross section including an optical path of the light from said light source unit to said image display light valve element, satisfying the following conditional expression (1) or (2):

$$f = \left\{ -L \pm L \left[1 + (\tan \theta)^2 \right]^{1/2} \right\} / 2 \tan \theta \qquad (1)$$

$$f = L/2 \tag{2}$$

where

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 $\theta \neq 90 + 180n$ (n being an integer) degrees in conditional expression (1);

 $\theta = 90 + 180n$ (n being an Integer) degrees in conditional expression (2);

f is the focal length of the parabolic mirror (where f > 0);

L is the distance between the optical axis of luminous flux before reflection and z axis of the parabolic mirror; and

- θ is the optical axis bending angle caused by reflection of the parabolic mirror.
- An illumination optical system according to claim 1, wherein said 5. curved surface is a hyperbolic mirror.
- An/illumination optical system according to claim 5, wherein said 6. hyperbolic mirrof has a form, in a cross section including an optical path of the light from said light/source unit to said image display light valve element, satisfying the following conditional expression (3):

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$$z = C\rho^2 / [1 + (1 - KC^2 \rho^2)^{1/2}]$$
 (3)

where

z is the distance between the reflection point of the optical axis of luminous flux before reflection in the hyperbolic mirror and the tangent plane at the apex of the hyperbolic mirror;

 ρ is the distance between the reflection point of the optical axis of luminous flux before reflection and z axis of the hyperbolic mirror;

C is a value defined as $C = a/b^2$ by a (where a > 0) and b satisfying the following conditional expressions (3-1) and (3-2); and

K is a value defined as $K = -a/b^2$ by a (where a > 0) and b satisfying the following conditional expressions (3-1) and (3-2);

$$8za^{3} + 4(z^{2} + \rho^{2})a^{2} - 2zL^{2}a - z^{2}L^{2} = 0$$
 (3-1)

$$2(a^2 + b^2)^{1/2} = L (3-2)$$

where

L is the focus-to-focus distance of the hyperbolic mirror defined by the following conditional expression (3-3):

$$L = \{ [(Q - M)\sin\theta]^2 + [(P - M) - (Q - M)\cos\theta]^2 \}^{1/2}$$
 (3-3)

where

P is the focal length of the optical system upstream the hyperbolic mirror;

Q is the composite focal length of the optical system upstream the hyperbolic mirror and the hyperbolic mirror;

M is the distance from the optical system upstream the hyperbolic mirror to the hyperbolic mirror; and

 θ is the optical axis bending angle caused by reflection of the hyperbolic mirror.

- 7. An illumination optical system according to claim 1, wherein said curved mirror is a spherical mirror.
- 8. A projection type image display apparatus comprising the illumination optical system according to claim 1.

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